MONO AND MULTI BAND EBG STRUCTURES : A COMPARITIVE STUDY

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ABSTRACT

In the current paper, mono and multi EBG structures for wider bandwidth are presented. For every EBG mentioned in this paper, metallic patches of regular shapes are selected as unit elements and these patches are altered to get additional inductance and capacitance which provides lower cut-off frequency and large bandwidth. The surface wave attenuation of EBG structures are juxtaposed with conventional EBG of mushroom type. The variation of transmission response due to unit element size, via diameter and distance between unit elements is shown. Out of these proposed EBG’s the square patch is small, the fractal EBG has wider bandwidth. The square patch with mono disconnected loop type slot and the fractal are multi band. The designing of microwave circuits and the antennas can be done using these EBGs.

KEYWORDS

Microstrip line, EBG, surface waves , Patch, Mono Band and double-band

1. INTRODUCTION

Surface Waves are undesirable in any antenna design. The parameters like gain, radiation pattern and efficiency of the antenna are degraded by the surface waves as these waves travel along the surface plane. In antenna array design due to these waves mutual coupling is caused which produce blind scanning angles. The augmentation of the dielectric constant makes surface waves more dominant which can be observed in the MMIC RF circuits [1-6].UWB band pass filters are one of the widely used band pass filters due to their capability of high speed data transmission. However, their performance is affected by the surface waves as the surface waves produce spurious stop bands[7].Multilayer pcb’s also suffer from electromagnetic interference and signal integrity problems caused by stimulation of resonance modes by concurrent switching noise[8-10].

These issues can be resolved by the implementation of Electromagnetic Band gap structures. Electromagnetic band gap structures posses periodic metal patches on a dielectric substrate or a combination of dielectric only. EBG structures have a property of obstructing the surface waves at a specific frequency and also reflect back any incoming wave without any phase shift.. These characteristics of EBG structures enhance the characteristics of an antenna [1-3].Ebg’s are used for the enhancement of the gain, isolation and diversity gain in MIMO systems. Further they are used to obtain notched characteristic in Ultra Wideband Antenna[11] and suppression of noise and EMI in high speed circuits[12-15].Theoretical analyses and practical models are present in references[16-18].Large number of techniques are proposed on designing of dual band and multi band structures but they have a limitation of narrow bandwidth[19-22].In [19]To produce a heterogeneous band the a slot of double U type is prepared in the patch .In [20] a fractal structure creates a double band characteristic, where as a spiral type structure is utilized for creation of multiband characteristic.
In the present paper, mono band and double band EBG structures with wide bandwidth are proposed. To obtain double band EBGs the cyclical nature of micro strip circuits is utilized. Alternative circuits of the mentioned EBGs are also presented and also the transmission responses of the EBGs are juxtaposed with a traditional mushroom type EBG. In the second section, mono band EBGs are mentioned and explained whereas in the third section double band EBGs are mentioned. The FR-4 substrate having dielectric constant 4.4 is used as the material. These are used in high speed circuits for reduction of noise and EMI and in antennas for boosting the bandwidth, gain. The simulation of these EBG’s is done by the Ansoft HFSS and CST Microwave studio. The construction and testing of EBG’s is done to confirm the results.

2. SINGLE BANDEBG

Here, three types EBG’s namely the cross hair, Swastika and hexagonal patch are discussed and analysed through microstrip line method. The juxtaposition of EBG’s in the aspects of resonance frequencies and bandwidths is done with a conventional mushroom type EBG. The schematic of EBG is demonstrated in Figure 1 and it consists of two substrates, patch and via. The two extremes of the 50 ohms line are linked to two ports and the S21 is calculated using appropriate stimulation.

![Figure 1. Schematic of EBG](image)

**Mushroom Type EBG**

This is a three dimensional EBG with a cylindrical via. The transmission characteristics further relies upon the width of the substrate and its material. Fig. 1 demonstrates a mushroom type EBG and its alternative circuit model. Fig. 2 demonstrates the mushroom type EBG’s transmission response is altered with various patch sizes and the distance between the unit elements is considered to be 1 mm, the via diameter 0.6 mm and width of the substrate is 0.8 mm. It is clear from figure that an augmentation the patch size boosts the capacitance value and causes the shifting of the stop band towards the lower frequency side. The capacitance, inductance and resonance frequency are represented by (1), (2) and (3) respectively [2].

\[
C = \frac{Wg(1+\epsilon_{r})}{\epsilon_{r}} \cosh^{-1} \left(\frac{W+g}{g}\right) \quad (1)
\]

\[
L = 2 \times 10^{-7}h \left[\ln\left(\frac{2M}{r}\right) + 0.5 \left(\frac{2r}{M}\right) - 0.75\right] \quad (2)
\]

\[
f_{r} = \frac{1}{2\pi\sqrt{LC}} \quad (3)
\]
Where ‘W’ represents the side length of the patch, ‘g’ denotes the distance between the unit elements, ‘h’ denotes thickness of the substrate, ‘r’ denotes radius of the via, $\varepsilon_0$ and $\varepsilon_r$ denotes permittivity of free space and relative permittivity respectively.

![Image](image1.png)

Figure 1. (a) Mushroom type EBG (b) Equivalent circuit of Mushroom type EBG

![Image](image2.png)

Figure 2. Simulated transmission response of Mushroom type EBG for different element size (Substrate thickness=0.8 mm, via diameter =0.6 mm, Gap between unit elements=1 mm)

**Cross Hair Type EBG**

Fig. (3a) demonstrates a cross hair type EBG obtained by alteration of the mushroom type EBG having a patch and micro strip lines. An additional inductance than the mushroom type EBG is present due to micro strip lines. The diameter of the via is 0.6 mm.. Fig. (3b) demonstrates how the transmission response of this EBG is altered for various widths of the micro strip lines used. An augmentation in the width decreases the inductance value which makes the resonance frequency move towards the higher frequency region. Fig. 4 demonstrates the impact of the alteration of the separation ‘g’ of the unit elements on the transmission response of cross hair EBG. The reduction in separation of unit elements augments the capacitance value which causes the stop band to relocate towards the lower region. For maximum bandwidth, the ideal value of gap is found to be 0.8 mm.
Figure 3. Cross hair type EBG (a) Unit element (b) Effect of variation of the width ‘W’ of the microstrip line on the transmission response of the EBG (g=1 mm, unit element size =3 mm x 3 mm)

Figure 4. Effect of variation of gap between the unit elements ‘g’ on the transmission response (w=0.2 mm, Unit element size=3 mm x 3 mm)

Figure 5. Impact of unit element size on the transmission response (W=0.2 mm, g=0.8mm)

Swastika type EBG

This EBG produces capacitance due to which better resonance is generated than the cross hair. Figure (6a) demonstrates unit element of the swastika type EBG and a prototype. Figure (6b) demonstrates the alternate circuit. The swastika type EBG is prepared on the same substrate (FR-
4). The diameter of via is taken as 0.6 mm. Figure 7 demonstrates transmission response of the swastika type EBG. The calculated band of the swastika type EBG is relocating towards the higher frequency region; This phenomenon is due to the limitation of fabrication which keeps a small chasm between the EBG and the 50 ohm line. The transmission response and bandwidth of swastika type EBG desirable than the Mushroom and Cross hair EBG’s.

![Figure 6(a). Swastika Type EBG Unit element 6(b) Equivalent circuit](image)

![Figure 7. Different transmission responses of Swastika type EBG](image)

Figure 8. demonstrates how the alteration in width of strip g1 changes the transmission response. It can be observed from the figure that an augmentation in g1 causes the resonance frequency to relocate towards the higher frequency side due to reduction in the capacitance value. It is also analysed that as gap g1 augments, the bandwidth augments (if -15dB bandwidth is considered).

Figure 9. Demonstrates how the diameter variation impacts the transmission response of this EBG.
Figure 8. Impact of alteration of distance between the strips ‘g1’ on transmission response of Swastika type EBG (with w = 0.2 mm and s= 1 mm).

Figure 9. Impact of via diameter variation on transmission response of Swastika type EBG

Figure 10. Demonstrates transmission responses of the three EBGs. It is clear from the figure that the minimum frequency of operation and maximum bandwidth are possessed by the swastika type EBG. The Cross Hair type EBG has an advantage of lower frequency of operation compared to the mushroom type EBG.

Figure 10. Juxtaposition of transmission responses of mushroom type, Cross Hair type and Swastika type EBG
Hexagonal patch type EBG

In a mushroom type EBG instead of using a rectangular patch a hexagonal patch of side length 4mm and via diameter of 1.0mm is used. FR-4 of width 1.53mm is used as the substrate. Figure 11 (a) represents the model of EBG of hexagonal patch. Figure 11(b) demonstrates transmission response. The bandwidth obtained is 1 GHz (3.65 GHz to 4.65 GHz).

![Hexagonal patch type EBG](image)

Figure 11. Hexagonal patch type EBG (a) fabricated prototype and (b) Measured and Simulated transmission response.

<table>
<thead>
<tr>
<th>S.No.</th>
<th>TYPE OF EBG</th>
<th>LOWER CUT OFF FREQUENCY (Ghz)</th>
<th>Higher cut-off frequency (Ghz)</th>
<th>Bandwidth (GHz)</th>
</tr>
</thead>
<tbody>
<tr>
<td>1) Mushroom 3 mm x 3 mm</td>
<td>8.50</td>
<td>10.50</td>
<td>2.00</td>
<td></td>
</tr>
<tr>
<td>4 mm x 4 mm</td>
<td>6.64</td>
<td>7.96</td>
<td>1.32</td>
<td></td>
</tr>
<tr>
<td>5 mm x 5 mm</td>
<td>5.44</td>
<td>6.56</td>
<td>1.12</td>
<td></td>
</tr>
<tr>
<td>2) Cross Hair 3 mm x 3 mm</td>
<td>9.10</td>
<td>11.38</td>
<td>2.28</td>
<td></td>
</tr>
<tr>
<td>4 mm x 4 mm</td>
<td>6.18</td>
<td>7.36</td>
<td>1.18</td>
<td></td>
</tr>
<tr>
<td>5 mm x 5 mm</td>
<td>5.00</td>
<td>6.00</td>
<td>1.00</td>
<td></td>
</tr>
<tr>
<td>3) Swastika 3 mm x 3 mm</td>
<td>7.50</td>
<td>11.10</td>
<td>3.60</td>
<td></td>
</tr>
<tr>
<td>4) Hexagonal patch (8 mm x 8 mm)</td>
<td>3.26</td>
<td>4.93</td>
<td>1.67</td>
<td></td>
</tr>
</tbody>
</table>

Table 1 Cut-off frequencies and Bandwidths of mono band EBGs

From the table it can be inferred that the Swastika type EBG is better in the aspects of dimensions and bandwidth.
3. DOUBLE BAND EBG

The micro strip circuit is cyclical in nature. This attribute can be utilized to develop a double band EBG. Although a double band nature can be generated by all EBG’s, the dimensions and geometry play an important role to get double band in the required frequency range. Here, three different types of are fabricated for double band and their attributes are juxtaposed with a mushroom type EBG of similar dimensions. The transmission characteristics of a mushroom type EBG fabricated for double band and the transmission characteristic of solid ground is juxtaposed in Figure 11. Using mushroom type EBG’s of two different sizes (8 mm x 8mm and 6 mm x 6mm). The substrate has a width of 1.53 mm, via diameter is 1 mm and the distance between the unit elements is 1 mm. It is clear from the figure that an augmentation in the size of the EBG relocates the bands towards the lower frequency region because of augmentation in the capacitance.

![Figure 11. Juxtaposition of Simulated transmission response of solid ground and mushroom type EBGs of different size (Substrate thickness=1.53 mm, via diameter=1 mm, Gap between unit elements=1 mm)](image)

**Hexagonal patch (Double C Type Slot)**

Figure 12 (a) demonstrates EBG of ‘C’ type slot and Figure 12(b) demonstrates the transmission responses for various slot widths. It can be understood from Figure 12(b) that an augmentation in the slot width makes the band relocate towards the lower frequency region due to augmentation in inductance.

![Figure 12. Hexagonal patch with C type slot EBG (a) Unit element (b) Transmission response for different slot width.](image)
**EBG with Square patch of mono disconnected loop type slot**

Figure 13(a) demonstrates the unit element of this EBG. Slicing a slot in the patch generates an extra inductance and therefore it relocates the bands towards the lower frequency region. Figure 13(b) demonstrates the transmission responses. Figure 14 demonstrates how the width of slot impacts the transmission response of the EBG. It is clear from Figure 14 that an augmentation in the slot width makes the lower band relocates towards the lower frequency region.

![Figure 13. Square patch with single disconnected loop type slot type EBG (a) Unit element (b) Measured and simulated transmission response.](image)

Figure 14. Effect of slot width on transmission response of Square patch with single disconnected loop type slot EBG

The distribution of current in the EBG of disconnected loop type slot is demonstrated by Figure 15. The largest value of current density is denoted by red colour whereas the least value of the current density is denoted by blue colour. It is clear from the figure that at stop band frequencies of EBG, as the signal travels from one port to the other port it gets attenuated. At 6.0 GHz, the signal is not attenuated and the attenuation at 8.0 GHz is more compared to that of the attenuation at 3.6 GHz.
Figure 15. Distribution of current for a square patch at various frequencies

**EBG of fractal Type**

The Fabrication of fractal type ebg of unit element size 6mm*6mm is done. Figure 16 demonstrates the unit element of this EBG. It’s characteristics are more desirable than EBG. The minimized dimensions for the fractal EBG are X = 2 millimeters Y = 1.4 millimeters, A = B = 0.6 millimeters, g = 0.8 millimeters. The via diameter is 1.2 mm. Figure 17 demonstrates how the alteration in the width of slot changes the transmission response of the EBG. From Figure 17 it can be understood that after a specific value of slot width the band gets divided. The minimal value of the width of the slot is obtained as 1.4 mm and the lower frequency band is unaffected by the width of the slot and the impact of separation between unit elements is demonstrated by Figure 18. It is observed that the separation ‘g’ affects the higher band bandwidth. The ideal value of ‘g’ is obtained as 0.8 mm.

Figure 16. Fractal type EBG (a) Unit element (b) Transmission response comparison of fractal and conventional mushroom type element having equal unit element size.

Figure 17. Impact of slot width ‘y’ variation on transmission response of the fractal EBG (x = 2 mm, a = b = 0.6 mm, g = 0.5 mm)
From the table, it is verified that slicing a slot relocates the band to the lower frequency region thereby compactness can be obtained. For an ebg of mushroom type and fractal type the cut-off frequency and bandwidth for the lower band are equal. But, its bandwidth is more in the upper band than the mushroom type EBG.
4. CONCLUSIONS

Various Electromagnetic Band Gap Structures for mono and double band operation in the Ultra Wide Band region are scrutinized. An augmentation in the unit size causes the capacitance to increase which makes the stop band shift towards the lower frequency region due to an augmentation in the capacitance. Augmentation in the distance between the unit elements relocates the stop bands towards higher frequency region due to reduction in the capacitance. Augmentation in the via diameter reduces the inductance which in turn relocates the stop bands towards higher frequency region. Out of all single band EBGs, the swastika type EBG offers better performance in both compactness (lower resonance frequency) and bandwidth. Out of all double band EBGs the fractal type has better bandwidth. The proffered EBGs are used for boosting the gain of antenna bandwidth, signal integrity and obstruction of noise in fast switching circuits.

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REFERENCES


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